

Waveguide Slot Array Simulation

Slotted waveguide arrays consist of a number of slots cut into the walls of a waveguide forming an array with the slots acting as individual radiating elements.

The resonant slot array employs near half-wavelength long resonant slots as individual radiators. The array elements are excited in the standing wave mode, which is formed by a short circuit end of the waveguide.

The concrete design task here is a 10-element transversal slot array cut into the upper wide side of a WR-51 standard rectangular waveguide. The operating frequency is the center of the K band, 18.5 GHz. The dimensions of the waveguide cross-section are $A=0.51$ inch=12.95 mm, and $B=0.255$ inch=6.477 mm.

shown here for reasons of clarity, eventhough full radiation pattern was calculated.

Single Slot Simulation

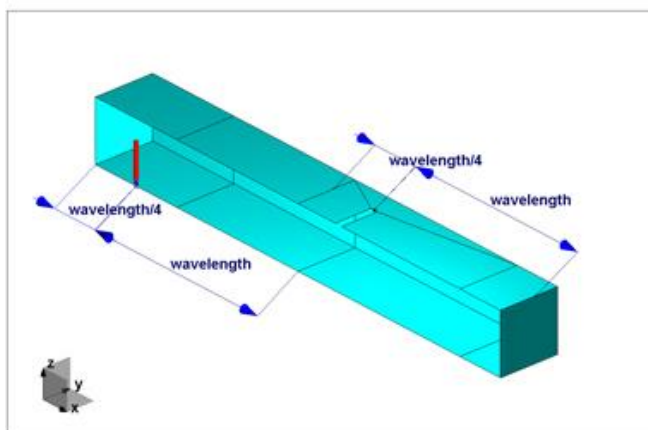


Fig.1. Model of one waveguide slot – one symmetry plane

TE_{10} waveguide mode is excited by a coaxial probe, modeled by a wire segment $\lambda/4$ from the waveguide end, as shown in Fig.1. Slot is cut into the waveguide at the point where surface currents would otherwise be longitudinal, at the upper side of the waveguide. Only half of the waveguide is modeled, due to symmetry. The complete model is shown in Fig.2.

The real part of the longitudinal component of the Poynting vector calculated along the axis of the waveguide shows the transfer of power from the generator to the slot (Fig.3). The first marker is set to the position of the wire-probe feeder, while the second marker is at the position of the center of the slot.

The radiation pattern (in dBi) of a single slot is shown in Fig.4. Only radiation pattern in half-space has been

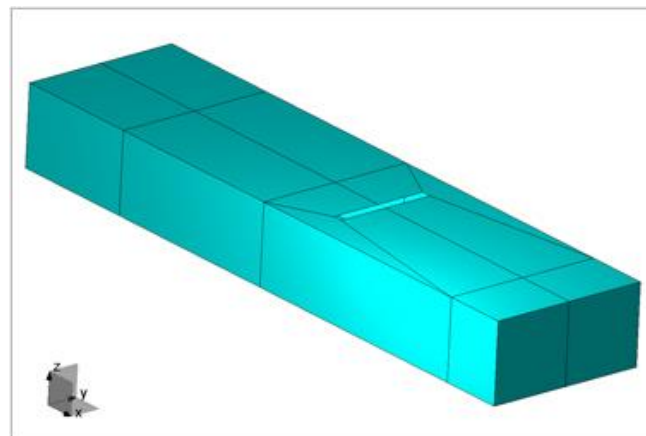


Fig.2. Complete model of waveguide slot

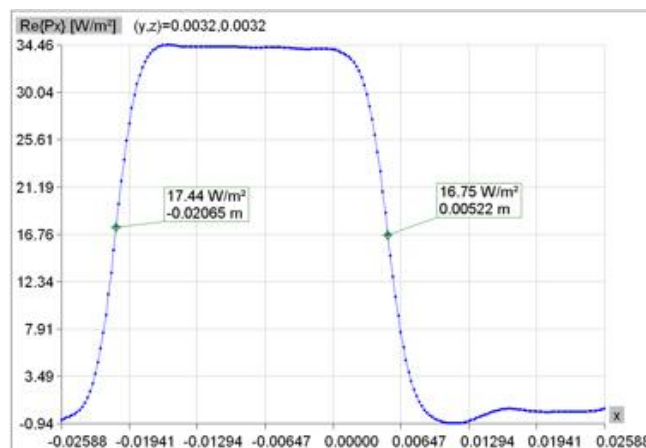


Fig.3. Real part of the Poynting vector longitudinal component along the axis of the waveguide (one slot)

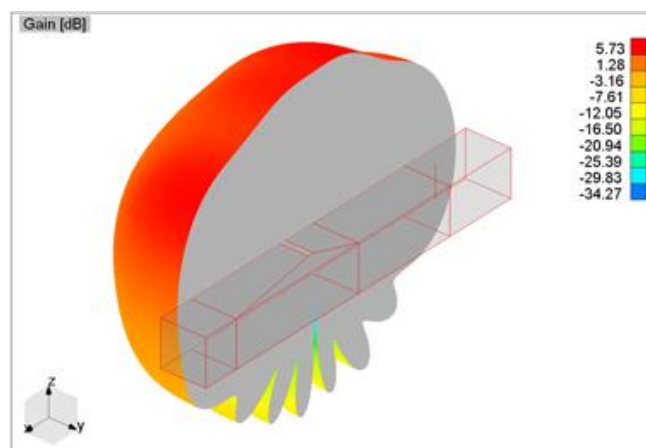


Fig.4. Radiation pattern in half-space of a single slot

This model requires only 444 unknowns thanks to higher order MoM applied in WIPL-D Pro 3D EM Solver and takes only 0.26 seconds to be solved. The simulation which includes calculation of radiation pattern in 32761 directions and near field in 209 points takes 7 seconds on an Intel(R) Core(TM) i7 Quad CPU with 3.07 GHz clock.

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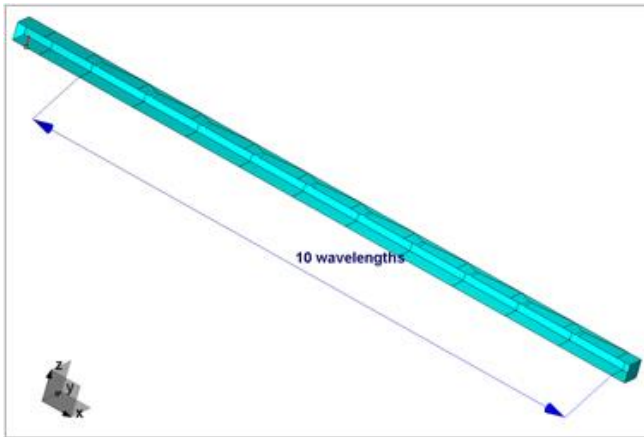


Fig.5. 10-element slot array model – one symmetry plane

The 10-element model is built by using the single slot model and applying a single *Copy* operation to create the other 9 array elements. The slots are positioned periodically at the points where surface currents would otherwise be longitudinal, at the upper side of the waveguide, one guide-wavelength apart. This distance enables in-phase excitation of all slots.

The real part of the longitudinal component of the Poynting vector calculated along the axis of the waveguide shows the transfer of power from the generator to the slots, with a part of power being radiated at each slot (Fig.6). The markers designate the positions of the generator and the fifth slot.

The radiation pattern (in dBi) of the slot array is shown in Fig.7. The gain is 14.8 dBi and the radiation

is broadside, with two pronounced grating lobes, which are expected since distance between array elements is one guide-wavelength.



Fig.6. Real part of the Poynting vector longitudinal component along the axis of the waveguide (array)

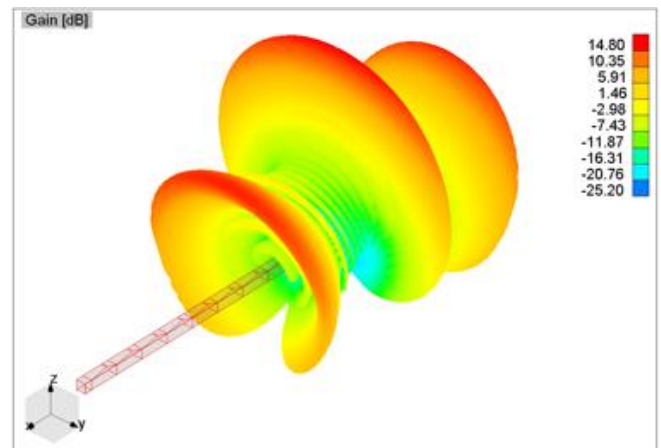


Fig.7. Radiation pattern of the array

The array model requires 2154 unknowns and is solved in 4.6 seconds. In case where calculation of radiation pattern in 32761 directions and near field in 209 points is included, the simulation lasts 14 seconds on an Intel(R) Core(TM) i7 Quad CPU with 3.07 GHz clock.

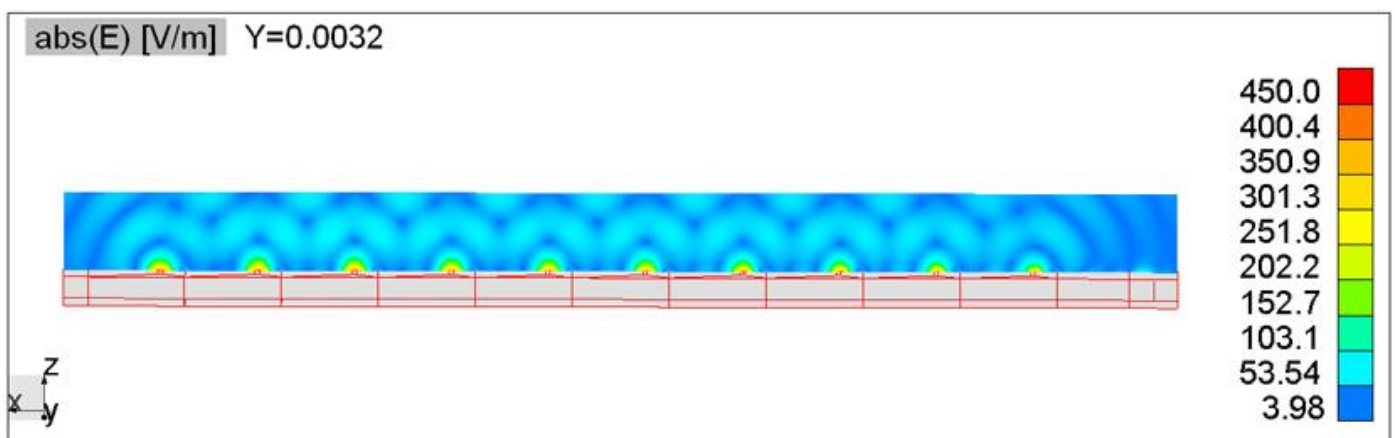


Fig.8. Near field in front of slots in case of 10-element array